Event	Date and venue	Further details from
34th IUPAC International Symposium on Macromolecules	13–18 July 1992 Prague, Czechoslovakia	IUPAC Macro 92 Secretariat, Institute of Macromolecular Chemistry, Czechoslovak Academy of Sciences, Heyrovského nám. 1888/2, 16206 Prague 6, Czechoslovakia
XIth International Congress on Rheology	17–21 August 1992 Brussels, Belgium	<b>Dr Paula Moldenaars,</b> Chemical Engineering Dept, Katholieke Universiteit Leuven, de Croylaan 46, B-3001 Leuven, Belgium
Solid State Devices and Materials	26–28 August 1992 Tsukuba Science City, Japan	SSDM '92 Secretariat, c/o Business Centre for Academic Societies Japan, Crocevia Blig. 2F, 3-23-1 Hongo, Bunkyo-ku, Tokyo 113, Japan
Crystallization of Polymers—a NATO Advanced Research Workshop	7–11 September 1992 <i>Mons, Belgium</i>	<b>Prof. M. Dosière,</b> NATO Advanced Research Workshop, Université de Mons-Hainaut, place du Parc, 20, B-7000, Mons, Belgium
Macromolecules '92	7–11 September 1992 Canterbury, UK	Dr Allan Amass, Macromolecules '92, Speciality Materials Research Group, Aston University, Aston Triangle, Birmingham B4 7ET, UK
Fourth Meeting on Fire Retardant Polymers	9–11 September 1992 Freiburg, Germany	<b>Prof. Dr Rolf Mülhaupt</b> , Institut für Makromolekulare Chemie, Stefan-Meier Str. 31, W-7800 Freiburg i.Br., Germany
Plastics in Telecommunications VI and Electrical, Optical and Acoustic Properties of Polymers III	16-18 September 1992 London, UK	Conference Secretariat, PIT VI/EOA III, The Plastics and Rubber Institute, 11 Hobart Place, London SW1W 0HL, UK
Thermal Degradation of Polymers: Techniques, Mechanisms and Stabilisation	16–18 September 1992 Cambridge, UK	<b>Professor N. S. Allen,</b> Department of Chemistry, Manchester Polytechnic, John Dalton Building, Chester Street, Manchester M1 5GD, UK
CONSTRUCTIONPLAS '92	20–22 October 1992 Arlington, VA, USA	Plastics Institute of America, 277 Fairfield Road, Suite 100, Fairfield, NJ 07004-1932, USA
Polypropylene World Congress	27-28 October 1992 Zürich, Switzerland	Moack Business Services, Plastics Technology and Marketing, CH-8804 Au/near Zürich, Switzerland
K'9212th International Trade Fair—Plastics and Rubber	29 October-5 November 1992 Dusseldorf, Germany	<b>Dusseldorf Trade Shows, Inc.,</b> 150 North Michigan Ave., Suite 2920, Chicago, IL 60601, USA
Plastics on the Road '92	30 November-1 December 1992 Solihull, UK	Conference Department. Plastics and Rubber Institute, 11 Hobart Place, London SW1W OHL, UK
Cellular Polymers III	23–25 March 1993 Edinburgh, UK	Kay Royle, Rapra Technology Ltd, Shawbury, Shrewsbury, Shropshire SY4 4NR, UK
4th International Conference on Polymers in Offshore Engineering	9–11 June 1993 Gleneagles, Scotland	Conference Secretariat, The Plastics and Rubber Institute, 11 Hobart Place, London SW1W OHL, UK

## Corrigendum

Kammer, H.-W. 'On the excess volume in polymer blends' *Polymer* 1991, 32, 501

The following corrections are necessary in the above paper.

Equation (7) must read

$$\begin{split} \langle \widetilde{V}_{i} \rangle (\langle \widetilde{T}_{i} \rangle) &= \langle \widetilde{V}_{AA} \rangle - \left( \frac{\partial \langle \widetilde{V}_{i} \rangle}{\partial \langle \widetilde{T} \rangle} \right)_{AA} \langle \widetilde{T}_{AA} \rangle (\mu - \mu^{2}) \\ &+ \frac{1}{2} \left( \frac{\partial^{2} \langle \widetilde{V}_{i} \rangle}{\partial \langle \widetilde{T} \rangle^{2}} \right)_{AA} \langle \widetilde{T}_{AA} \rangle^{2} \mu^{2} \quad (i = A, B) \end{split}$$

where

$$\mu \equiv \frac{\langle \varepsilon_i^* \rangle}{\langle \varepsilon_{AA}^* \rangle} - 1$$

Furthermore, the second expression in equation (15) must be replaced by

$$\left(\tilde{T}^{2} \frac{\partial^{2} \tilde{V}}{\partial \tilde{T}^{2}}\right)_{A} = 2 \frac{\left(\frac{14}{9} - \tilde{V}_{A}^{1/3}\right) (\tilde{V}_{A}^{1/3} - 1)^{2} \tilde{V}_{A}}{\left(\frac{4}{3} - \tilde{V}_{A}^{1/3}\right)^{3}}$$

Hence, for the volume of mixing, equation (16), it follows

$$\begin{split} \frac{\Delta \widetilde{V}^{E}}{\phi_{A}\phi_{B}\widetilde{V}_{A}} &= \frac{3}{4}\rho \left(\Gamma + \frac{11}{2}\rho\right) \\ &+ \frac{\widetilde{V}_{A}^{1/3} - 1}{\frac{4}{3} - \widetilde{V}_{A}^{1/3}} \left(2X_{AB} - \frac{3}{4}\Gamma^{2} + 9\rho^{2} + \frac{9}{4}\rho\Gamma\right) \\ &- \frac{\left(\frac{14}{9} - \widetilde{V}_{A}^{1/3}\right)\left(\widetilde{V}_{A}^{1/3} - 1\right)^{2}}{\left(\frac{4}{3} - \widetilde{V}_{A}^{1/3}\right)^{3}} \frac{3}{4}\Gamma^{2} \end{split}$$

The curve in Figure 1 results with the parameters  $X_{\rm AB}=-1\times 10^{-4},~\Gamma^2=1\times 10^{-4},~\phi_{\rm A}=0.5$  and  $\tilde{V}_{\rm A}^{1/3}=1.082$ .